Moisture dependent thermal properties of cassia

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Bhupendra M. Ghodki¹, A.D. Srikanth Tangirala¹ and T.K. Goswami¹*

Abstract: Thermal and mechanical properties of cassia are primarily required in the study of its different thermal and mechanical operations. The thermal properties of cassia bark viz., specific heat, glass transition temperature ($T_g$), bulk thermal conductivity, and bulk thermal diffusivity were determined for a moisture range of 8–14% dry basis (d.b). Compression test was performed by Universal Testing Machine to examine the breaking characteristics of cassia along its three orthogonal directions at 11.10% d.b. moisture level. Results revealed that the specific heat increased from 1,553.12 to 3,232.90 J kg⁻¹ °C⁻¹ with an increase in moisture at 30°C. Whereas $T_g$ decreased linearly from −66.67 to −86.09°C and the bulk thermal conductivity increased linearly from 0.10 to 0.14 W m⁻¹ °C⁻¹ with a rise in moisture content of the sample. Moreover, the bulk thermal diffusivity of cassia bark decreased from 2.75 × 10⁻⁷ to 1.62 × 10⁻⁷ m² s⁻¹ with an increase in moisture level. The average rupture forces for cassia bark through the minor axis, major and intermediate axis were 0.130, 0.123 and 0.109 kN, respectively, and corresponding average deformations at rupture were 1.36, 1.30 and 0.91 mm, respectively. In conclusion, the thermal properties of cassia were significantly affected by the variation in the moisture level. Also, the mechanical properties such as rupture force and rupture deformation demonstrated a prominent difference in their values along the three axes of the sample.

Subjects: Biophysics; Food Science & Technology; Processing

Keywords: cassia; specific heat; glass transition temperature; bulk thermal conductivity; rupture force

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1. Introduction
Spices are one of the essential agricultural commodities that perform a crucial role in our present day life as a flavoring and preserving agent in foods, including pharmaceuticals and cosmetic applications (Ghodki & Goswami, 2016a, 2016b, 2016c, 2016d). Cinnamon and cassia are the dried bark of evergreen trees belonging to genus *Cinnamomum* which has 250 species, and most of them are aromatic and flavoring. A classification system in these spices has evolved by the country of origin and climatic conditions in which they are grown because each type has distinctive flavoring characteristics. Hence, cinnamon and cassia have been separated into two distinct species in the past: *Cinnamomum verum* Presl L. as cinnamon; while, *Cinnamomum cassia* Presl L., *Cinnamomum loureirii* Nees L., *Cinnamomum burmannii* Blume L. are considered as cassia (Ghodki & Goswami, 2015; Tainter & Grenis, 2001). Ceylon Cinnamon or true cinnamon is the most common name of the cinnamon in Spice Industry which is indigenous to Sri Lanka; while cassia may be grown in Indonesia, China, Vietnam, and India (Peter, 2006).

Cassia (*Cinnamomum loureirii* Nees L.) belongs to the family of Lauraceae commonly known as Saigon or Vietnamese Cassia, native to Vietnam, and is one of the major economic species of *Cinnamomum* (Goswami & Ghodki, 2015; Peter, 2006). Vietnam’s annual export of cassia bark is about 2,000 to 3,000 tons, which is 8–10% of world trade (Iqbal, 1993). Further, Cassia is known for its higher volatile oil content and sweeter flavor (Ghodki & Goswami, 2016d).

The knowledge of mechanical and thermal properties is necessary for engineering as well as in the process design such as simulation and modeling of heat transfer in the freeze dryer, cold storage, grinders and cooling system for a cryogenic grinder. The heat generated in the conventional grinding technique is detrimental to the spice (cassia) powder quality (Ghodki & Goswami, 2015). Further, the thermo-mechanical properties of spices are preliminary requirements for thermal analysis of the mechanical processes involving heating or cooling. For example, the heat transfer modeling techniques like Discrete Element Modeling and Computational Fluid Dynamics requires the sample (spice) properties such as specific heat, thermal conductivity, stress, etc. as a set of input data to model the thermal transport phenomena of a mechanical process such as grinding. Further, the thermal analysis of the grinding operation would help in understating the heat generation mechanism in the process. Moreover, it is essential to know and interpret the thermal and mechanical properties of the biomaterials at various stages of the production, processing, and preservation. In agricultural materials, thermal properties are significantly influenced by the change in moisture (Mohsenin, 1980). Also, mechanical properties of cassia are vital in the design of size reduction operation such as grinding. Hence, the objectives of this study are: (1) To investigate the effect of moisture content on thermal properties of cassia; (2) To determine the influence of compression along the orthogonal axes of the sample on its breaking characteristics.

2. Materials and methods

2.1. Raw material
Cassia bark (*Cinnamomum loureirii* Nees L.) was procured from Tien Thanx Trading and Production Co. Ltd., Hamo commune village, Dan Phuong district, Hanoi city, Vietnam. The cleaned cassia bark was broken into small pieces of length less than or equal to 50 mm for analysis of the thermal properties and breaking characteristics (Ranganna, 1986).

2.2. Moisture content
Moisture content of the sample was measured by entrainment method as recommended in US ISO 939 (Klimánková et al., 2008). Moisture level range of 8–14% d.b. was selected (8, 10, 12, and 14% d.b.) each with a standard deviation of ± 0.1% d.b. to study the influence of moisture on thermal properties of cassia. A similar procedure was adopted to maintain and preserve the sample at different moisture levels as reported in the author’s previous study (Ghodki & Goswami, 2015). Proper care was taken to check the moisture content of the sample before determination of the properties.
(Altuntaş & Yıldız, 2007; Singh & Goswami, 1996). Five replicates were taken for all the moisture levels, and average values are reported.

### 2.3. Specific heat and glass transition temperature

Differential scanning calorimetry (DSC) (Model Pyris Diamond DSC, Perkin Elmer, USA) was used for the measurement of specific heat at −90 and 30°C along with glass transition temperature (\(T_g\)). The Diamond DSC was controlled by Pyris Software (Version: 8.0.0.0172, Perkin Elmer, USA) via a temperature control program. The specific heat and \(T_g\) of a sample were measured experimentally, after calibration the DSC with a thermally and chemically inert standard Indium (−156.90°C peak) of known mass and specific heat, according to the manufacturer’s specification to obtain an accuracy level of ±1%. About five cassia barks were selected randomly from each moisture levels for their thermal analysis. The DSC sample (cassia bark) was taken as small pieces of 1–1.2 mm length and weighed accurately (6–8 mg) in an open aluminium pan (30 μL) and placed in a DSC module with a reference pan (same empty aluminium pan). Both the pans were capped with an aluminium cap and sealed to restrict any changes during the experimentation process (heating/cooling). The temperature range of DSC analysis was −160 to 65°C at a steady heating rate of 10°C min⁻¹. Moreover, the DSC thermogram was observed as an output of the test. The ordinate of the thermogram represents the rate of heat evaluation/absorption while the abscissa of thermogram provides a measure of temperature or time. Further, the thermogram was analyzed for specific heat and \(T_g\) by the Pyris Software. The rate of heat flow in the sample was proportional to its specific heat and displacement of the sample run from the baseline was measured to determine the specific heat (Dodd, Tonge, & Currell, 1987). While \(T_g\) was determined as the midpoint of the temperature range at which changes in heat capacity thermogram occurs (Ibrahim, Zakaria, Sipaut, Sulaiman, & Hashim, 2011). Moreover, thermal parameters viz., Peak temperature (Tpeak), onset temperature (Tonset), endset temperature (Tendset), and change in specific heat (Δ\(C_p\)) were calculated for heating sweeps. The properties analyzed by DSC in the lower temperature regime would be helpful in the study of the operations such as cryogenic grinding, cryogenic freezing, freeze drying, etc.

### 2.4. Bulk thermal conductivity

Transient-hot-wire method was used for determination of the bulk thermal conductivity of the cassia. “This approach involves a thin heating wire located at the interface between the sample and a reference of known thermal conductivity” (Sahin & Sumnu, 2006). The temperature of the thin heating wire increased when the electric power was applied continuously to the wire which was stretched straight through a rectangular sample. A Quick Thermal Conductivity Meter (QTM-D3, Kyoto Electronics Manufacturing Co. Ltd., Japan) (Meghwal & Goswami, 2011) was used for determination of the bulk thermal conductivity of the samples at 30 ± 1°C with an accuracy of ±5% reading value per reference plate. The average values of five replicas at each moisture level are reported.

### 2.5. Bulk density

Bulk density of the cassia at different moisture levels (8, 10, 12, and 14% d.b.) were determined using a circular container of volume \(1.482 \times 10^{-3} \text{ m}^3\), which was filled with cassia sample to its full volume and was gently tapped with proper care to avoid compaction of cassia in the container. Bulk density was calculated as the ratio of the weight of the sample to the volume of the container (Ghodki & Goswami, 2016c). Five replicates were taken at all moisture contents, and the average values are reported.

### 2.6. Bulk thermal diffusivity

Bulk thermal diffusivity of cassia was computed using experimental values of bulk density, specific heat and bulk thermal conductivity using Equation (1) as reported by (Aviara, Haque, & Ogunjimi, 2008).

\[
\alpha_b = \frac{k_b}{\rho_b C_p}
\]  

(1)
where $\alpha_b$ is the bulk thermal diffusivity ($\text{m}^2\text{s}^{-1}$); $k_b$ is the bulk thermal conductivity ($\text{W m}^{-1}\text{C}^{-1}$); $C_p$ is the specific heat ($\text{J kg}^{-1}\text{C}^{-1}$); $\rho_b$ is the bulk density ($\text{kg m}^{-3}$).

2.7. Dimensions
The average dimensions of cassia barks were determined at the initial moisture level of 11.10% d.b. along the three orthogonal axes of cassia using dial calipers (Mitutoyo Corporation, Japan) reading to an accuracy of $\pm 0.02$ mm. Twenty samples were randomly selected from the moisture resistant polyethylene bag to determine principal dimensions, namely major (length, L), intermediate (width, B) and minor (thickness, T) axes, respectively, measured at three different points of the respective dimensions, viz., two endpoints and a midpoint. After determining the dimensions, the same samples were tested to determine the mechanical properties.

2.8. Mechanical properties
The breaking characteristics viz., average rupture force (peak load) and average deformation (peak deformation) at rupture were investigated at three loading position at a moisture level of 11.10 $\pm$ 0.1% d.b. as shown in Figure 1. A Twin-column Universal Tester (UTM) (UTB9052, Dak System Inc., India) was used to perform the tests. The samples with minimal defects like cracks (observed by a magnifying glass) were taken for the analysis. Dak System Inc. Software was used to control the UTM as well as to analyze the results. Compression test was performed along three orthogonal axes of the sample by UTM equipped with a 4,905 N load cell (Cárcel et al., 2012) and a crosshead speed of 1 mm min$^{-1}$ was kept constant throughout the test. A similar experimental procedure was followed as reported for determination of breaking characteristics of Shea kernel (Manuwa & Muhammad, 2011).

Figure 1. Representation of axial forces $F_x$, $F_y$ and $F_z$ acting along major, intermediate and minor axis respectively; the three axes and three perpendicular dimensions of cassia bark: X-axis, longitudinal axis (major axis, length, L); Y-axis, transverse axis containing the intermediate dimension (intermediate axis, width, W) at right angles to the longitudinal axis; Z-axis, transverse axis containing the minor dimension (minor axis, thickness, T).
The output of the test was in the graphical form of the force-deformation (load-deformation) curve as shown in Figure 2 for a sample. Parameters like rupture force which corresponds to a bio-yield point in force-deformation curve and deformation at rupture were recorded and reported. The UTM also provides the actual values of rupture force and deformation via the analysis software. The measurement accuracy of UTM was ±0.0001 N for force and 0.0001 mm for deformation.

2.9. Statistical analysis

The results observed were subjected to analysis of variance and Duncan test to evaluate for statistical significance of observed differences among treatment means using statistical software SPSS 20.0 (IBM Corporation, USA). Origin 2015 (OriginLab Corporation, USA) data analysis and graphing software was used for analysis of regression and plotting graphs. Statistical significance was expressed at 95% (p ≤ 0.05) confidence interval.

3. Results and discussion

Thermal properties of cassia obtained from experimentation are shown in Table 1. The initial moisture level measured in the sample was 11.10 ± 0.1% d.b. The findings of thermal and mechanical properties are discussed in detail in this section.

<table>
<thead>
<tr>
<th>Thermal properties</th>
<th>Moisture content (%) d.b.</th>
</tr>
</thead>
<tbody>
<tr>
<td></td>
<td>8</td>
</tr>
<tr>
<td>Bulk thermal conductivity at 30°C (W m⁻¹ °C⁻¹)</td>
<td>0.10±&lt;0.01</td>
</tr>
<tr>
<td>Specific heat at 30°C (J kg⁻¹ °C⁻¹)</td>
<td>1,553.12±1.13</td>
</tr>
<tr>
<td>Specific heat at −90°C (J kg⁻¹ °C⁻¹)</td>
<td>1,486.09±1.02</td>
</tr>
<tr>
<td>Bulk thermal diffusivity at 30°C (m² s⁻¹)</td>
<td>2.75×10⁻⁹±1.83×10⁻⁹</td>
</tr>
<tr>
<td>Glass transition temperature (°C)</td>
<td>−86.09±0.90</td>
</tr>
</tbody>
</table>

Notes: Mean values of five samples in same row followed by italicized letters (a–d) are significant different (p ≤ 0.05); values are reported as mean ± standard deviation.
3.1. Bulk thermal conductivity

Figure 3 shows the influence of moisture level on the bulk thermal conductivity. It can be examined that the bulk thermal conductivity increased linearly with the moisture content at an average sample temperature of 30 ± 1°C. This increase could be because of the fact that the moisture has a higher bulk thermal conductivity than that of air, which may have replaced the air present in the void space of cassia. Similar trend was reported for sorghum (Sharma & Thompson, 1973), guna seed (Aviara et al., 2008), black pepper (Meghwal & Goswami, 2011) and cashew kernel (Bart-Plange, Addo, Kumi, & Piegu, 2012). Moreover, the values of bulk thermal conductivity varied from 0.10 to 0.14 W m⁻¹ °C⁻¹ (p ≤ 0.05) with moisture level ranging from 8 to 14% d.b. as shown in Table 1. Based on the experimental data, the relationship between moisture content and bulk thermal conductivity can be represented by Equation (2):

\[ K_b = 0.006 M + 0.057 \quad (R^2 = 0.986) \]  

where \( k_b \) is the bulk thermal conductivity of cassia (W m⁻¹ °C⁻¹); \( M \) is the moisture content (% d.b.); \( R^2 \) is the coefficient of determination.

3.2. Specific heat

Specific heat of cassia bark has shown an increase with temperature at specified moisture content and also with the moisture at a particular temperature. The specific heat followed the second order polynomial relationship with the moisture level at a particular temperature. The results are consistent with the report of different biomaterials such as cumin seed (Singh & Goswami, 2000), soybean (Deshpande & Bal, 1999), guna seed (Aviara et al., 2008) and black pepper (Meghwal & Goswami, 2011). The specific heat of the cassia bark increased from 1,486.09 to 3,232.90 J kg⁻¹ °C⁻¹ (p ≤ 0.05) with a rise in temperature from −90 to 30°C for a moisture range of 8.0–14.0% d.b. However, at −90°C, the specific heat increased from 1,486.09 to 3,096.44 J kg⁻¹ °C⁻¹ with an increase in moisture level. Whereas at 30°C it has risen from 1,553.12 to 3,232.90 J kg⁻¹ °C⁻¹ (p ≤ 0.05) as shown in Figure 4.

Moisture has a higher specific heat than that of air which was present in internal voids that may be one of the reasons for such an outcome.

Based on the experimental data, the specific heat of cassia as a function of moisture content at 30°C and −90°C can be expressed by Equations (3) and (4), respectively, which indicates a second order polynomial relationship of specific heat with the moisture level of cassia.

\[ C_{p30} = 75.62M^2 - 1395.98M + 7918.38 \quad (R^2 = 0.955) \]  

\[ C_{p(-90)} = 91.74M^2 - 1771.76M + 9854.01 \quad (R^2 = 0.870) \]
where $C_{p30}$ is the specific heat of cassia at 30°C (J kg$^{-1}$ °C$^{-1}$); $C_{p(-90)}$ is the specific heat of cassia at −90°C (J kg$^{-1}$ °C$^{-1}$); $M$ is the moisture content (% d.b.); $R^2$ is the coefficient of determination.

### 3.3. Bulk thermal diffusivity

The bulk thermal diffusivity decreased with the increase in moisture level and followed a second order polynomial relationship. A reduction in the value of bulk thermal diffusivity may be due to the increase in bulk density and specific heat was relatively higher than that of bulk thermal conductivity with the increasing moisture level. Similar results were reported for cumin seed (Singh & Goswami, 2000) and black pepper (Meghwal & Goswami, 2011). The bulk thermal diffusivity at 30°C varied from $2.75 \times 10^{-7}$ to $1.62 \times 10^{-7}$ m$^2$ s$^{-1}$ (p ≤ 0.05) with an increase in moisture level as shown in Figure 5. Based on the experimental data, Equation (5) could be used to express the relationship between the bulk thermal diffusivity of the cassia bark and its moisture content.

\[
\alpha_b = -5 \times 10^{-9}M^2 + 1 \times 10^{-7}M - 2 \times 10^{-7} \quad (R^2 = 0.985)
\]  

(5)

where $\alpha_b$ is the bulk thermal diffusivity of cassia at 30°C, m$^2$ s$^{-1}$; $M$ is the moisture content, % d.b.; and $R^2$ is the coefficient of determination.
3.4. Glass transition temperature

The magnitude of $T_g$ decreased linearly with increase in moisture level, resulting in a maximum glass transition temperature at the lowest moisture content (Figure 6) which could be due to the plasticizing effect of water on the amorphous constituent of cassia. The results are consistent with the report of osmo-dehydrated apple and pear (Mrad, Bonazzi, Courtois, Kechaou, & Mihoubi, 2013) and strawberries (Roos, 1987). The peak value of $T_g$ decreased from $-66.67$ to $-86.09$°C ($p \leq 0.05$) with the rise in moisture level of the sample. A typical DSC thermogram of cassia sample at a moisture content of 14% d.b. is shown in Figure 7. Based on the experimental data, Equation (6) could be used to express the relationship between $T_g$ of the cassia bark and its moisture content.

$$T_g = -3M - 42.80 \quad (R^2 = 0.913)$$

(6)

where $T_g$ is the glass transition temperature of cassia (peak value), °C; $M$ is the moisture content, % d.b.; $R^2$ is the coefficient of determination.
3.5. Mechanical properties

Dimensional properties of the cassia bark were determined at the moisture content of 11.10% d.b. which is presented in Table 2. Length (46.94 to 40.89 mm), width (17.69 to 13.55 mm) and thickness (2.72 to 2.48 mm) of cassia bark showed a non-significant change with the position.

The resistance of cassia bark to damage was presented in terms of the mean rupture force and the average deformation at rupture along the three orthogonal directions as shown in Table 2. Moreover, it can be observed that the mean rupture force of 0.130 kN was highest for the minor axis (along the thickness) as compared to the other two directions. The reason for such a result being as cassia bark compressed between the compression plates the bark may become flat after a few moment; hence, the force goes on increasing and ultimately leads to rupture. Average deformation at rupture of 1.357 mm was highest for the minor axis as compared to other two directions (Table 2), which may be due to the uneven surface of cassia bark along the minor axis. The results are in good agreement with the report of safflower seed (Baümler, Cuniberti, Nolasco, & Riccobene, 2006).

4. Conclusions

The outcomes of this research showed that change in moisture level of cassia from 8 to 14% d.b. caused a significant variation in its thermal properties such as bulk thermal conductivity, glass transition temperature, bulk thermal diffusivity and specific heat. The findings also presented that breaking resistance of the sample varied when tested along different orientations under compression.

The bulk thermal conductivity of cassia bark increased linearly with a rise in moisture content at 30°C. Moreover, the specific heat increased with increase in moisture at both the lower (−90°C) and the higher (30°C) temperatures. However, the bulk thermal diffusivity and glass transition temperature decreased with the rise in moisture level at 30°C. Differences between the mean values of all the thermal properties are statistically important at $p \leq 0.05$. The understanding of the thermal properties of cassia in such a lower temperature regime would be helpful in the studies involving design/heat transfer analysis of a system in the cryogenic regime such as cryogenic grinding system, cryogenic freezer, etc. Further, for cryogenic grinding of cassia, it could be better to use cassia samples at a moisture level of 14% d.b. that also provides an ease to achieve the brittleness of the cassia. However, to support this proposal process optimization is suggested based on the quality of ground cassia. Under compression, the average rupture force of cassia bark was in the range of 0.130 to 0.109 kN of which higher values of rupture force were obtained along the minor axis of cassia bark, while the smallest values of rupture force were obtained along the major axis. It implies that cassia bark offers less resistance to rupture along major axis as compared to the other two axes. While in the case of rupture deformation, higher values were obtained along the minor axis of cassia bark, whereas the smallest values of rupture deformation has been achieved along the major axis. Hence, while considering the design parameters of a cassia grinder this upper and lower limits of rupture force are important for the design of the system.
force and deformation at rupture should be considered along with other product, process, and machine parameters. The understanding of moisture dependent thermal properties helps to visualize the complex changes in cassia as well as in selecting suitable thermal processing conditions.

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Competing Interests
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